Job No. : 16036 Date: April 2017

Respond! Housing Association

Residential Development at Flinters Field, Athy, Co. Kildare

Engineering Report



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Contents Amendment Record

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1 INTRODUCTION

1.1 Introduction

Malone O'Regan have been commissioned by the applicant, The Respond! Housing Association to prepare a planning submission in respect of a proposed residential development at Flinters Field, Athy, County Kildare.

The purpose of this document is to outline the engineering proposals associated with the new development. The proposed development is fully described on the drawings which accompany this planning submission. Where reference is made to drawings and drawing numbers within this report these should be taken as meaning those drawings produced by Malone O'Regan unless specifically stated otherwise.

1.2 Project Description

The proposed development comprises the construction of 35 no. terraced, detached, semi-detached and terraced properties along with all associated infrastructure works including internal roads, footpaths, foul and surface water drainage pipework, surface water attenuation, a water supply network, landscaped play area and all other required services.

The proposed development is to be located adjacent to an existing residential development which was constructed by Respond in 2001. This previous development comprises a number of semi-detached residential properties and a community hall located along two residential streets known as Flinters Place and Flinters Close.

It is intended that vehicular access to the site will be via Flinters Place in the northern corner of the site and Flinters Close in the western corner of the site. A separate pedestrian link to Woodstock St to the northeast of the site is also proposed. The proposed road layout will also allow for a possible future road linkage in the southern corner of the site.

1.3 Site Location

The proposed development is to be located on a 1.9534ha greenfield site approximately 500m to the northwest of Athy town centre. The site is bordered to the north, south and east by other existing residential developments. The Grand Canal runs along the western boundary of the site. The River Barrow is located approximately 350m to the northeast of the site.





Figure 1.1 Location of the proposed development.

1.4 References

Reference has been made to the following publications in the preparation of this report.

- Greater Dublin Regional Code of Practice for Drainage Works, Version 6.0.
- Greater Dublin Strategic Drainage Study.
- EPA Wastewater Treatment Manuals, Treatment Systems for Small Communities, Business, Leisure Centres and Hotels.
- Planning Systems and Flood Risk Management: Guidelines for Planning Authorities November 2009.
- Design Manual for Urban Roads and Streets

2 SURFACE WATER DRAINAGE DESIGN

2.1 Proposed Layout

The proposed surface water drainage layout is indicated on drawing 16036/102. It is proposed to discharge all surface water runoff from the site into an existing surface water drain located in the northwestern portion of the site.

Surface water runoff from the new road surfaces and the roofs of the new buildings will be collected by gullies and directed towards two separate attenuation tanks. The outfall from each attenuation tank will be controlled using a Hydrobrake and the total surface water discharge rate will be limited to the 'greenfield' runoff value for the site.

All surface water drainage will be designed in accordance with the Greater Dublin Regional Code of Practice for Drainage Works.

2.2 Attenuation / Runoff Calculations

Development Area Details

Total Area = 19,534 m2 (1.9534 hectares)

	Area (m²)	Permeability Factor	Impermeable Area (m ²)
Roofs	2105	0.95	2000
Roads	3380	0.90	3042
Other Hardstanding	3525	0.80	2820
Grass	10524	0.10	1052
		Total Imp. Area =	8,914 m2

Calculation of Impermeable area:

Rainfall Data

The rainfall data used was based on Met Eireann Rainfall Data for Athy. The rainfall data and drainage criteria employed are as follows:

M5 - 60 = 15.8mm (Max. rainfall in 1 hour for 5 year return period)

M5 - 2D = 48.4mm (Max. rainfall in 2 days for 5 year return period)

Ratio, r = 0.33 (M5 - 60/ M5 - 2D)

Standard Average Annual Rainfall (SAAR) = 825mm

When calculating the required size of attenuation tank using Micro Drainage, an additional 10% was added to the above rainfall intensities to account for the future effects of climate change.

Permissible Runoff

The permissible rate of surface water runoff from the site has been taken as 2 litres per second per hectare. Given the site area of 1.9534 hectares, the allowable discharge rate is therefore 3.90 litres/s.

Attenuation Design & Outflow Connection

Calculations for the design of the attenuation tank are provided in Appendix A. These calculations are based on the design parameters listed above. The attenuation tank has been sized to cater for a 1 in 100 year storm event.

The required attenuation volume has been calculated using industry-standard design package Micro Drainage. The calculations provided in Appendix A show that the total volume of attenuation storage required on the site is 400m³.

Two separate attenuation tanks will be provided. The area of impermeable surfacing draining into each tank has been calculated. The attenuation tank located on the western side of the site, in front of house numbers 08 - 10 will receive 52% of the total runoff from the site. The other attenuation tank, located beside house number 02, will receive 48% of the total site runoff. Each tank has been sized to provide a volume in excess of $400m^3 \times 52\% = 208m^3$.

Each tank will have a storage capacity of **212m³**. The outflow from each tank will be limited to half of the total permissible runoff i.e. **1.95 l/s**.

3 FOUL WATER DRAINAGE DESIGN

3.1 Proposed Layout

It is proposed to provide foul drainage pipework to serve the development as indicated on drawing 16036/103. This new pipework will connect into an existing sewer which was installed as part of the previous Respond! Development on the adjoining lands. The existing sewer runs across the site from the western corner towards Woodstock St. It is proposed to connect the new pipework into this existing sewer at three separate locations.

All foul water drainage will be designed in accordance with the Greater Dublin Regional Code of Practice for Drainage Works.

Note Further information is requested from the Local Authority for the drainage in the neighbouring housing estates (St Dominic's Park and Cardington Crescent). This information may lead to changes in the site levels on the south east side.

3.2 Foul Discharge Calculations

The average and peak discharge rates were calculated using loading rates provided by Irish Water:

Dry Weather Flow (DWF) = 600 litres per dwelling (Source: Irish Water Pre-Connection Enquiry Form)

Number of properties = 35.

Total DWF = 600 x 35 = 21,000 litres / day = 0.243 l/s

Peak Discharge = $6 \times DWF$ = 6×0.243 = 1.46 l/s

4 WATERMAINS

4.1 Proposed Layout

The proposed watermain layout is indicated on drawing 16036/104 which accompanies this planning submission. It is proposed to provide new lengths of HDPE watermain to serve the development. The new watermains will be fed off an existing watermain which was installed as part of the previous Respond! development on the adjoining lands.

4.2 Water Demand Calculations

The average and peak water demand rates were calculated in accordance with the Irish Water Pre-Connection Enquiry Form which assumes a loading rate of 150 litres / person / day and an average occupancy ratio of 2.7 persons per dwelling. The average day, peak week demand is taken as 1.25 times the average daily domestic demand. The peak demand is taken to be 2.1 times the average day, peak week demand.

Number of properties = 35

Average Daily Domestic Demand = 150 x 35 x 2.7	= 14,175 litres / day
	= 0.164 l/s

Average Day Peak Week Demand = 0.164 x 1.25 = 0.205 l/s

Peak Demand	= 0.205 x 2.1
	= 0.431 l/s

Normal Demand (assuming principal water usage over 8 hrs) = 0.205 x 24/8 = 0.615 l/s

5 ROAD NETWORK

5.1 Internal Road Network

The internal road layout is indicated on drawing 16036/101. It is proposed to connect the new sections of carriageway to the existing roadways located within the previous Respond! development on the adjoining lands. A swept path analysis has been conducted and is shown on drawing 16036/105. It can be seen that emergency vehicles and bin lorries are able to safely manoeuvre around the proposed site layout.

A pedestrian footpath is proposed alongside the internal road network. Dropped kerbs and tactile paving will be provided at all pedestrian road crossing points. A pedestrian link to Woodstock St to the northeast of the site is also proposed.

All proposed roads, footpaths will be fully designed to meet the requirements of the Design Manual for Roads and Streets.

6 FLOOD RISK ASSESSMENT

The following sources of information were reviewed in order to identify any flood risk to the proposed development site:

- OPW Flood Records from www.floodmaps.ie
- The National Preliminary Flood Risk Assessment (PFRA) Overview Report & Indicative Flood Maps (OPW, March 2012, www.cfram.ie)
- The Planning Systems and Flood Risk Management: Guidelines for Planning Authorities; Technical Appendices November 2009

6.1 OPW Flood Records

An examination was made of the OPW Flood Records (www.floodmaps.ie). There are no recorded flood events in the vicinity of the site.

6.2 The National Preliminary Flood Risk Assessment

A further source of information used to establish the risk of flooding on the site is the flood maps contained within the OPW Catchment Flood Risk Assessment and Management (CFRAM) Study.

The relevant CFRAM maps indicating the extent of flooding caused by a fluvial flood event with an annual exceedance probability (AEP) of 10% (10yr event), 1% (100yr event) and 0.1% (1000yr event) are included in Appendix B.

An extract from these maps is provided in Figure 6.1 below. The light blue hatching indicates the areas which could be affected by flooding during an event with a 0.1% (1,000-yr event) annual exceedance probability. The proposed development site is indicated with a red boundary.

16036

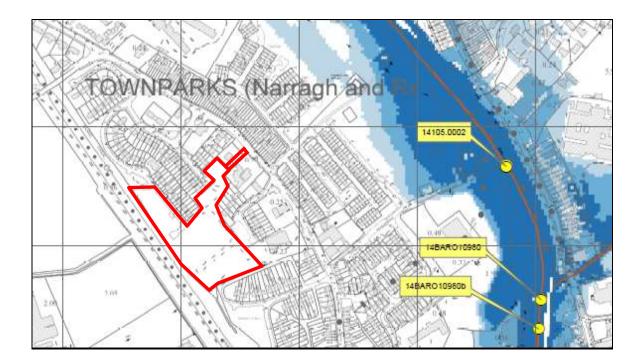


Figure 6.1 – Extract from PFRA Maps

From Figure 6.1 and the maps in Appendix B it can be seen that the site is predicted to remain unaffected by the most extreme 1 in 1000 year flood events. Flooding appears to be limited to the areas immediately alongside the River Barrow.

6.3 Sequential Approach to Flood Risk Management

The document "Planning Systems and Flood Risk Management: Guidelines for Planning Authorities November 2009" requires the adoption of a sequential approach to flood risk management when assessing the location for new developments. This approach is a risk-based method to guide development away from areas that have been identified through flood risk assessment as being at risk from flooding. The philosophy used in this approach is outlined in figure 6.2 below.

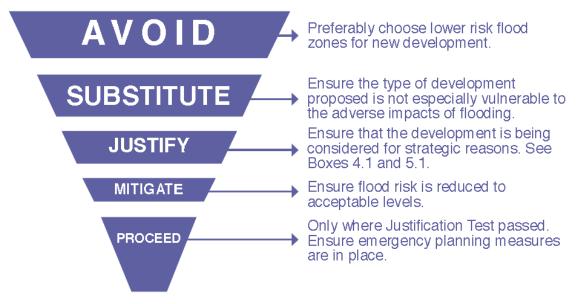


Figure 6.2 Source: The Planning Systems and Flood Risk Management: Guidelines for Planning Authorities November 2009

The sequential approach uses mapped flood zones alongside considerations of the vulnerability of different types of development to give priority to development in zones of low flood probability.

6.3.1 Flood Zones

The flood zones are defined on the basis of flooding from rivers and the sea. The different flood zones recommended in the 2009 Planning Guidelines are:

- **Flood Zone A** Highest risk area where there is a 1% chance of flooding in any one year from rivers and a 0.5% chance of flooding from the sea.
- **Flood Zone B** Moderate risk area where the chance of flooding in any one year is 0.1-1% for rivers and 0.1-0.5% for coastal flooding.
- **Flood Zone C** Low risk area with less than 0.1% chance of flooding from rivers or the sea in any given year.

As described in Section 6.2 above, the flood maps contained within the CFRAM Study indicate that the site is not predicted to flood even during the most extreme (1 in 1000 year) flood events. The development is therefore located within Flood Zone C.

6.3.2 Vulnerability Class of Proposed Development

The vulnerability class of the development is dependent on the land use and type of development proposed. See Figure 6.3 for the vulnerability classes.

Vulnerability class	Land uses and types of development which include*:
Highly vulnerable	Garda, ambulance and fire stations and command centres required to be operational during flooding;
development (including	Hospitals;
essential	Emergency access and egress points;
infrastructure)	Schools,
	Dwelling houses, student halls of residence and hostels;
	Residential institutions such as residential care homes, children's homes and social services homes;
	Caravans and mobile home parks;
	Dwelling houses designed, constructed or adapted for the elderly or, other people with impaired mobility; and
	Essential infrastructure, such as primary transport and utilities distribution, including electricity generating power stations and sub-stations, water and sewage treatment, and potential significant sources of pollution (SEVESO sites, IPPC sites, etc.) in the event of flooding.
Less vulnerable	Buildings used for: retail, leisure, warehousing, commercial, industrial and non-residential institutions;
development	Land and buildings used for holiday or short-let caravans and camping, subject to specific warning and evacuation plans;
	Land and buildings used for agriculture and forestry;
	Waste treatment (except landfill and hazardous waste);
	Mineral working and processing, and
	Local transport infrastructure.
Water-	Flood control infrastructure;
compatible development	Docks, marinas and wharves;
development	Navigation facilities,
	Ship building, repairing and dismantling, dockside fish processing and refrigeration and compatible activities requiring a waterside location;
	Water-based recreation and tourism (excluding sleeping accommodation);
	Lifeguard and coastguard stations;
	Amenity open space, outdoor sports and recreation and essential facilities such as changing rooms; and
	Essential ancillary sleeping or residential accommodation for staff required by uses in this category (subject to a specific warning and evacuation plan).
"Uses not listed here	should be considered on their own merits

Figure 6.3 Classification of Vulnerability to Flooding for Various Development Types

(Source – Table 3.1 Planning System and Flood Risk Management – Guidelines for Planning Authorities DEHLG, OPW, November 2009)

The proposed development includes 35 no. properties which will be used as private dwellings. It therefore constitutes a "highly vulnerable development".

The 2009 Planning Guidelines presents a matrix of vulnerability versus flood zone to illustrate appropriate development and the requirement of justification tests. That matrix can be seen in Figure 6.4. The proposed development is classified as a highly vulnerable development from Figure 6.3 and it is located within Flood Zone C. The development is therefore considered appropriate with regards to the anticipated flood risk and no further justification test is required.

	Flood Zone A	Flood Zone B	Flood Zone C
Highly vulnerable development (including essential infrastructure)	Justification Test	Justification Test	Appropriate
Less vulnerable development	Justification Test	Appropriate	Appropriate
Water-compatible development	Appropriate	Appropriate	Appropriate

Figure 6.4 - Matrix of Vulnerability vs. Flood Zone

(Source – Table 3.1 Planning System and Flood Risk Management – Guidelines for Planning Authorities DEHLG, OPW, November 2009)

APPENDIX A – ATTENUATION CALCULATIONS

Microstrain Ltd		Page 1
Unit B3	Athy Housing	
Metropoint Business Park	SC740 @ 100YRP +10%	4
Swords Co. Dublin	3.541/s	Micco
Date 15/12/16	Designed by JM	
File	Checked by	Digitigh
XP Solutions	Source Control 2015.1	,

Summary of Results for 100 year Return Period (+10%)

Half Drain Time : 1166 minutes.

	Stor Even		Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control (1/s)	Max Σ Outflow (1/s)	Max Volume (m³)	Status
15	min N	Winter	0.380	0.380	0.0	2.4	2.4	145.9	ОК
30	min N	Winter	0.508	0.508	0.0	2.4	2.4	195.1	ОК
60	min N	Winter	0.636	0.636	0.0	2.6	2.6	244.0	ОК
120	min N	Winter	0.765	0.765	0.0	2.9	2.9	293.9	ОК
180	min N	Winter	0.840	0.840	0.0	3.0	3.0	322.7	ОК
240	min N	Winter	0.891	0.891	0.0	3.1	3.1	342.0	ОК
360	min N	Winter	0.956	0.956	0.0	3.2	3.2	367.2	ОК
480	min N	Winter	0.995	0.995	0.0	3.3	3.3	382.1	ОК
600	min N	Winter	1.019	1.019	0.0	3.3	3.3	391.1	ΟK
720	min N	Winter	1.032	1.032	0.0	3.3	3.3	396.4	ОК
960	min N	Winter	1.042	1.042	0.0	3.4	3.4	400.0	ОК
1440	min N	Winter	1.030	1.030	0.0	3.3	3.3	395.7	ОК
2160	min N	Winter	1.000	1.000	0.0	3.3	3.3	384.1	ОК
2880	min N	Winter	0.957	0.957	0.0	3.2	3.2	367.4	ОК
4320	min N	Winter	0.861	0.861	0.0	3.1	3.1	330.6	ОК
5760	min N	Winter	0.768	0.768	0.0	2.9	2.9	294.9	ОК
7200	min N	Winter	0.682	0.682	0.0	2.7	2.7	261.7	ΟK
8640	min N	Winter	0.601	0.601	0.0	2.6	2.6	230.9	ОК

	Storm Event	Rain (mm/hr)		Discharge Volume (m³)	Time-Peak (mins)
15	min Winter	80.534	0.0	139.8	19
30	min Winter	54.133	0.0	181.1	33
60	min Winter	34.245	0.0	247.9	62
120	min Winter	21.049	0.0	304.0	122
180	min Winter	15.710	0.0	339.3	180
240	min Winter	12.729	0.0	365.1	238
360	min Winter	9.448	0.0	401.9	354
480	min Winter	7.635	0.0	424.8	470
600	min Winter	6.468	0.0	435.8	584
720	min Winter	5.646	0.0	439.0	694
960	min Winter	4.554	0.0	441.2	908
1440	min Winter	3.362	0.0	443.0	1142
2160	min Winter	2.480	0.0	652.0	1604
2880	min Winter	1.999	0.0	699.2	2076
4320	min Winter	1.474	0.0	753.1	2980
5760	min Winter	1.187	0.0	834.8	3856
7200	min Winter	1.002	0.0	881.4	4688
8640	min Winter	0.873	0.0	921.1	5528
	©19	82-2015	XP Sol	utions	

Microstrain I	Ltd								Page 2
Unit B3				Athy	Housir	ıg			-
Metropoint Bu	usiness Pa	ırk) YRP +10%	5		4
Swords Co. I				3.54					
Date 15/12/10					gned by	7 JM			
File					ked by				Drainage
XP Solutions						rol 2015	5.1		
	Summary o	of Resu	lts f	for 10	00 year	Return	Period	(+10%))
	Storm Event	Level D	Max epth (m)	Infilt		Max Control Σ (1/s)		Max Volume (m³)	Status
10080	min Winter	0.526 0	.526		0.0	2.4	2.4	201.8	O K
		Storm Event			Flooded Volume (m³)	Discharge Volume (m³)	e Time-P (mins		
	10080	min Wint	ter	0.777	0.0	955.2	2 6	352	
		C	982	-2015	XP Sol	utions			

Microstrain Ltd		Page 3
Unit B3	Athy Housing	
Metropoint Business Park	SC740 @ 100YRP +10%	<u> </u>
Swords Co. Dublin	3.541/s	Micco
Date 15/12/16	Designed by JM	
File	Checked by	Drainage
XP Solutions	Source Control 2015.1	
<u></u> <u></u> <u></u>	infall Details	
Rainfall Model	FSR Winter Storms Y	es
Return Period (years)	100 Cv (Summer) 0.7	50
Region Scotla	and and Ireland Cv (Winter) 0.8	40
M5-60 (mm)	15.800 Shortest Storm (mins)	15
Ratio R	0.330 Longest Storm (mins) 100	
Summer Storms	No Climate Change % +	10

<u>Time Area Diagram</u>

Total Area (ha) 0.873

Time	(mins)	Area	
From:	To:	(ha)	

0 4 0.873

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Microstrain Ltd	Page 4	
Unit B3	Athy Housing	
Metropoint Business Park	SC740 @ 100YRP +10%	4
Swords Co. Dublin	3.541/s	Micco
Date 15/12/16	Designed by JM	
File	Checked by	Drainage
XP Solutions	Source Control 2015.1	I

Model Details

Storage is Online Cover Level (m) 2.000

Cellular Storage Structure

Invert Level (m) 0.000 Safety Factor 2.0 Infiltration Coefficient Base (m/hr) 0.00000 Porosity 0.60 Infiltration Coefficient Side (m/hr) 0.00000

Depth (m) Area (m²) Inf. Area (m²) Depth (m) Area (m²) Inf. Area (m²)

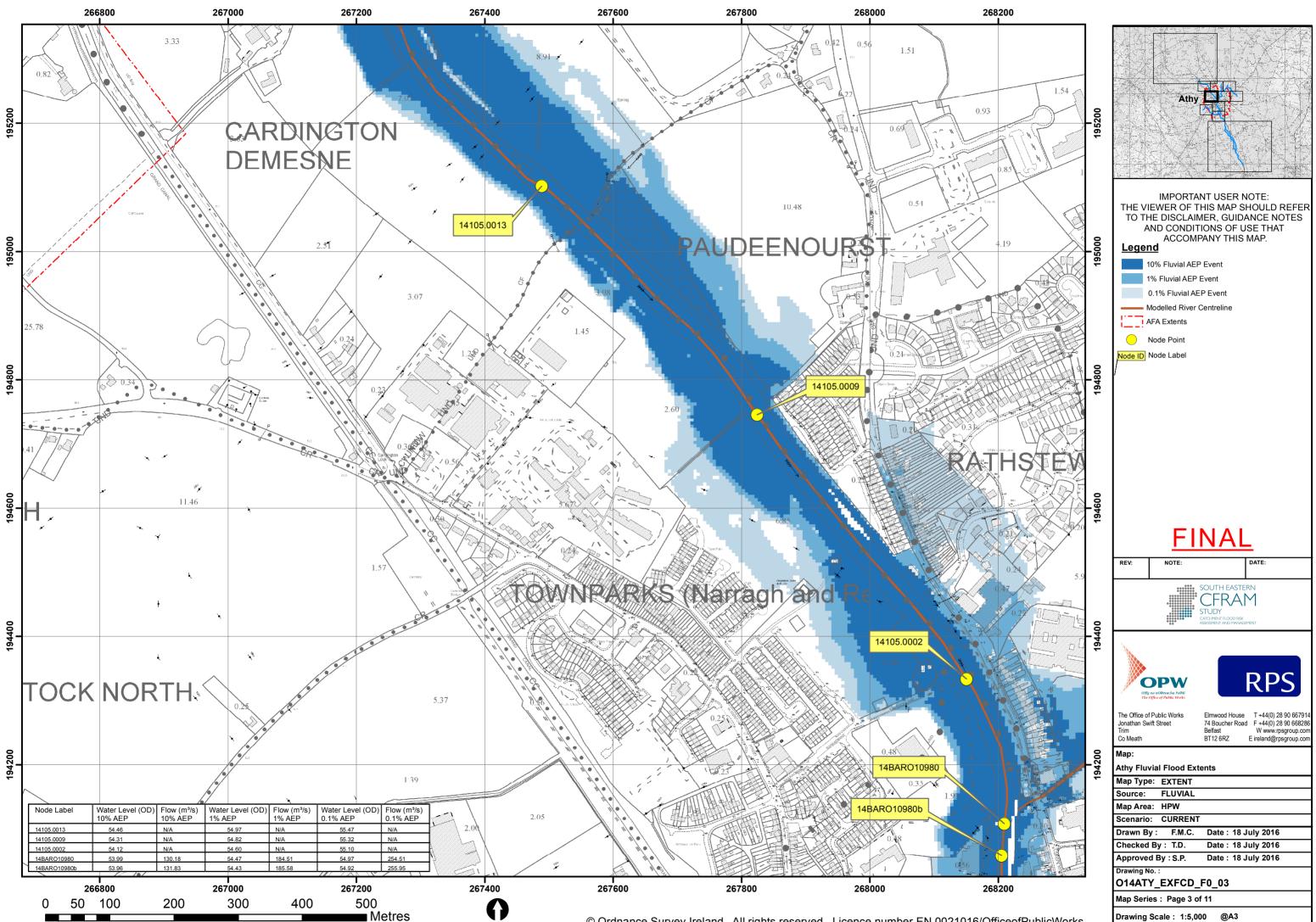
0.000	640.0	640.0	1.200	0.0	754.4
1.100	640.0	754.4			

Hydro-Brake® Outflow Control

Design Head (m) 1.100 Hydro-Brake® Type Md6 SW Only Invert Level (m) 0.000 Design Flow (1/s) 3.5 Diameter (mm) 76

Depth (m) Flow	(l/s)	Depth (m) Fl	Low (l/s)	Depth (m) Flow	(l/s)	Depth (m)	Flow (l/s)
0 1 0 0		1 000	2.5	0.000			0.5
0.100	2.0	1.200	3.6	3.000	5.7	7.000	8.7
0.200	2.4	1.400	3.9	3.500	6.2	7.500	9.0
0.300	2.2	1.600	4.2	4.000	6.6	8.000	9.3
0.400	2.2	1.800	4.4	4.500	7.0	8.500	9.6
0.500	2.4	2.000	4.7	5.000	7.4	9.000	9.9
0.600	2.6	2.200	4.9	5.500	7.7	9.500	10.2
0.800	3.0	2.400	5.1	6.000	8.1		
1.000	3.3	2.600	5.3	6.500	8.4		

APPENDIX B – CFRAM FLOOD MAPPING



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